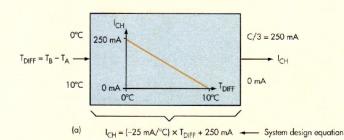
"Intelligent" NiCd Charger Avoids Battery Damage From High Currents

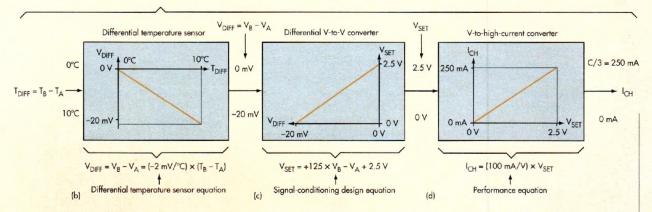
ROBERT S. VILLANUCCI AND JOSEPH DIECIDUE

WENTWORTH INSTITUTE OF TECHNOLOGY, BOSTON, MASS. villanuccir@wit.edu, dieciduej@wit.edu

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I. These graphs and equations represent the battery-protection circuit's operation, including the overall design (a), the temperature sensor circuitry (b), the differential-voltage-to-voltage converter (c), and the voltage-to-high-current converter (d).



Care must be exercised when you try to "quickly" charge a nickel-cadmium (NiCd) cell or battery pack at a current density that approaches or exceeds one-third of its capacity (C/3). As the battery becomes fully charged, the high charging current raises both the internal cell pressure and temperature, which can quickly degrade the battery or destroy it.

One way to avoid damage is to monitor the differential temperature ($T_{\rm DIFF}$) between the battery's surface temperature ($T_{\rm B}$) and the ambient ($T_{\rm A}$) and to proportionally reduce the charging current ($I_{\rm CH}$) as the differential temperature increases. Of course, you must make sure that the sensor monitoring the ambient environment is attached to a structure that approximates the thermal mass of the battery pack. Otherwise, the resulting difference in thermal delays will adversely affect results.

Consider an example design that must convert a differential temperature ranging from 0°C to 10°C into a charging current that decreases proportionally from C/3 to 0 A. If C equals 750 mA, C/3 equals 250 mA and the equation to describe this linear system is:

$$I_{CH} = \left(-25 \frac{\text{mA}}{^{\circ}\text{C}}\right) T_{DIFF} + 250 \text{ mA}$$
 (1)

Figure 1 represents this design equation (Fig. 1a), including graphical and mathematical descriptions of the main circuit elements: temperature sensor circuitry (Fig. 1b), a differential-voltage-to-voltage converter (Fig. 1c), and a voltage-to-high-current converter (Fig. 1d). The circuit measures the two relevant temperatures, T_B and T_A , individually using two matched low-cost silicon-diode temperature sensors.

The sensor outputs, V_B and V_A , are applied to the inputs of a differential amplifier that subtracts, scales, and offsets these voltages, producing a single-ended control voltage (V_{SET}) that's inversely proportional to T_{DIFF} . Finally, a voltage-to-high-current converter delivers the needed charging current (I_{CH}), which is directly proportional to V_{SET} .

ROBERT VILLANUCCI, professor, holds an AEng from Wentworth Inst., Boston, Mass., a BSET from Northeastern Univ., and an MSEE from Tuffs Univ., Medford, Mass.

JOSEPH DIECIDUE electronics technician, holds a BSEE from Wentworth Institute, Boston, Mass.



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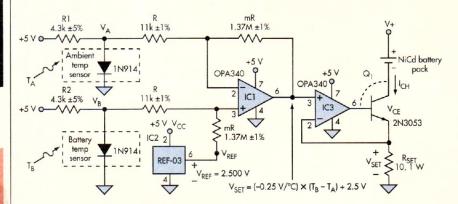
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2. The voltage outputs of the temperature-sensing diodes are applied to a standard difference amplifier, which in turn outputs the difference voltage that will vary from -20 V to 0 V as the difference temperature rises from 0°C to 10°C.

Figure 1 shows that at a T_{DIFF} of 0°C $(V_{DIFF} = 0 \text{ V})$, V_{SET} is chosen to be 2.5 V and will set the maximum charging current of 250 mA. When the TDIFF rises to 10°C $(V_{DIFF} = -20 \text{ mV})$, V_{SET} will have linearly dropped to 0 V, causing I_{CH} to drop to 0 and charging to cease.

The design begins by writing three linear equations that describe each of the circuit elements depicted graphically. The two temperature-derived diode voltages (Fig. 2) are applied to the inputs of a standard difference amplifier (IC1), which subtracts sensor voltage $V_A = (-2 \text{ mV/}^{\circ}\text{C})T_A + 670$ mV from $V_B = (-2 mV/^{\circ}C)T_B + 670 mV$ to produce a differential voltage (V_{DIFF}):

$$V_{DIFF} = V_B - V_A = \frac{-2 \text{ mV}}{{}^{\circ}\text{C}} (T_B - T_A)$$
 (2)

In addition to performing the subtraction described by Equation 2, IC, amplifies VDIFF by a differential gain (ADIFF), determined to be 125, and adds an offset voltage of +2.5 V to the output. The differential amplifier's performance equation is:

$$V_{\text{SET}} = A_{\text{DIFF}} \left(V_{(+)} - V_{(-)} \right) + V_{\text{REF}}$$
 (3)

The components are selected by simply comparing gain and offset terms to design the needed signal-conditioning circuit described by:

$$V_{SET} = +125(V_B - V_A) + 2.5 V$$
 (4)

Notice that comparing terms also shows how to correctly wire the inputs—i.e., V_B

must be wired to the V(+) input and VA must be wired to the $V_{(-)}$ input. IC_1 's differential gain is:

$$A_{DIFF} = \frac{mR}{R} \qquad (5)$$

V_{REF} is set by IC₂, a low-output-impedance reference chip (a REF-03) that creates precisely 2.50 V.

The design of the voltage-to-highcurrent converter starts by noting that ICH is directly proportional to the temperaturedependent voltage, V_{SET}, and circuit performance is:

$$I_{CH} = \frac{100 \text{ mA}}{V} V_{SET}$$
 (6)

Finally, note that negative feedback around IC3 forces VSET to be applied directly across the current-setting resistor, R_{SET} making:

$$R_{SET} = V_{SET}/I_{CH} = 2.5 \text{ V}/250 \text{ mA} = 10 \Omega$$

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